



Article Dirac-Based Quantum Admittance of 2D Nanomaterials at Radio Frequencies

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Abstract: Starting from a rigorous finite mass, Dirac equation-based model, we investigate the R.F. quantum admittance of a monolayer 2D material under the action of an electromagnetic (e.m.) wave with axially directed vector potential. With some reasonable approximations, the analysis yields a relatively simple RLC-equivalent circuit with frequency-independent elements depending on the bias, temperature, effective mass, Fermi velocity and effective e.m. index of the material, losses and other relevant parameters.

Keywords: Dirac equation; quantum admittance; graphene nanoribbons

1. Introduction

The drive toward circuit miniaturization and the advent of new materials, such as graphene, has led to a situation where the quantum current flows on mesoscopic and nanoscopic conductors. The quantum current and conductivity in nanostructures present novel and interesting aspects that have been the subject of much interest in recent years. In evaluating this kind of situation with a finite electron mass, the Schrödinger equation from quantum mechanics has been used in the framework of a free electron model, where electrons are described by scalar wave functions. This description is, however, incomplete when the polarization and magnetization aspects become important (e.g., in the common situation of applied electromagnetic fields). In such a case, the use of a four-component Dirac spinor description becomes necessary. In a conductor in particular, the scalar ratio between the first pair of components and the second pair plays the role of characteristic impedance of a transmission line, where the ratio of source impedance to load impedance is essential for the correct definition of transmittivity. In a previous work [1], we derived from the Dirac equation with a finite effective mass the quantum current in the presence of a d.c. electric field parallel to the surface of a 2D nanomaterial and, consequently, the d.c. conductivity. In the literature, a large number of works address the problem of charge transport in low-dimensional structures and related applications [2–25]. In this work, we consider the action of an R.F. electric field in the same idealized 2D geometry. In the case of a device with dimensions much smaller than the electromagnetic wavelength, the electromagnetic boundary conditions of the field can be neglected, and the tensor character of the admittance can be approximated as scalar since the cross-impedance effect is low. Real loss mechanisms, such as intra-band transitions and interaction with the substrate, are subsumed by a global, finite mean free path L_F . Our aim is to extend the calculation of the scalar quantum conductivity previously performed in the d.c. case to the case of the R.F. admittance. The amplitude of the driving R.F. field is assumed initially to not be depleted by losses and be unaffected by the current on the surface (low loss approach). Once the current has been evaluated, losses are introduced in the potential, leading to the complex R.F. admittance at the signal frequency. The intensity of the R.F. signal is assumed to be moderate enough to not affect the electron density or Fermi distribution, and its action is assumed to start at x = 0 and t = 0.



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2. Dirac Equation

Considering the problem in Figure 1, the Dirac equation in x and t, with a finite effective mass m_e and Fermi velocity v_F in the band of interest, is

$$\left[v_F \alpha_x (-i\hbar\partial_x + |e|\mathbf{A}) + \beta m_e v_F^2\right] \Psi = [i\hbar\partial_t + |e|\Phi] \Psi$$
(1)

where $|e|\Phi$ stands for the energy related to the total scalar potential Φ , which is due to the d.c. electric field as well as that associated with the vector potential A. When dealing with the modulation of a time harmonic, namely a very high frequency carrier (e.g., optical) by a radio frequency (R.F.), it is expedient to separate the large but constant contribution of the carrier frequency ω_c from that of the time modulation by writing

$$\partial_t = -i\omega_c + \partial_\tau. \tag{2}$$

In the present case, the "rest" energy is

$$m_e v_F^2 = 2E_F \tag{3}$$

where in the case of parabolic dispersion, in absence of doping and identifying m_e with the cyclotron mass, it is usually much larger than all other contributions. It is therefore appropriate to extract from the Hamiltonian on the RHS of Equation (1) its stationary terms by rewriting it as

$$i\hbar\partial_t = m_e v_F^2 + E' + i\hbar\partial_\tau \tag{4}$$

where τ is the time scale of the modulation and E' is the stationary state energy we are considering. Clearly, we have to integrate over the range of possible E' values. Schrödinger's equation is actually recovered from Equation (1) by repeated application of the Hamiltonian operator in the limit $m_e v_F^2 \gg E'$, neglecting the squares of the potentials and passing from a spinor to a scalar wave function by equating the currents. Moreover, we have in Equation (1) that

$$V = V_0 + E_0 x \tag{5}$$

$$\Phi = V + \phi(x, \tau) \tag{6}$$

where V_0 is the d.c. bias constant in space and time, E_0 is the constant d.c. field, if any, and ϕ is the time-dependent scalar potential associated with the vector potential A such that the Lorentz gauge is satisfied:

$$\nabla \cdot A + \frac{1}{v^2} \partial_\tau \phi = 0 \tag{7}$$

In our case, by disregarding transverse variation over the ribbon width $(2\pi/k \gg L_y)$, where *k* is the wavenumber in the media) and boundary conditions of the e.m. field, we assume an x-directed vector potential

$$\boldsymbol{A} = \hat{A}e^{i(k_x x - \omega\tau)} \hat{\boldsymbol{x}}$$
(8)

that implies a scalar potential $\phi = -(v^2/\omega)k_x \hat{A}e^{i(k_xx-\omega\tau)} = -n_e vA$, where $n_e = k_x/k_0$ is the "effective" "index" of the propagating wave. The Dirac equation (Equation (1)) is now cast in the working form

$$\left[\alpha_{x}\left(\partial_{x}+i\frac{|e|}{\hbar}A\right)-i\frac{|e|}{\hbar}\frac{\phi}{v_{F}}+\frac{1}{v_{F}}\partial_{\tau}\right]\Psi=\frac{i}{\hbar v_{F}}\left[\left(E'+E_{v}+m_{e}v_{F}^{2}\right)I-m_{e}v_{F}^{2}\beta\right]\Psi\tag{9}$$

where I is the 4 × 4 identity matrix and $E_v = |e|V$ is the d.c. field energy. As mentioned, we also subsume constant small losses (e.g., due to interaction with the substrate) over a finite mean free path L_F , leading to a propagation decay of the type e^{-x/L_F} , simply by replacing ∂_x with $\partial_x \pm 1/L_F$ according to whether the wave is progressive or regressive. This modification keeps the remainder of the equation Hermitian in nature. The solution

of the system of the partial differential equation (Equation (9)) is uniquely determined by the initial and boundary conditions. A proper definition of quantum admittance also requires no return wave and a proper input match at the origin of the computational domain ($0 \le x \le L_x$) for a progressive wave traveling from left to right.



Figure 1. Representation of the domain under study, showing the adopted sign convention. Electric potential and current density present opposite directions, which explains the negative sign in the admittance definition in Equation (37).

3. Spinor Solution

As a preliminary, E_V is assumed to be constant either in absence of the d.c. field or following a stepwise approximation of V for modest fields. This expedience allows us to eliminate the inconvenient, constant diagonal matrix on the RHS of Equation (9) by means of a similarity transformation:

$$\Psi' \equiv \begin{bmatrix} \sqrt{E' + E_V}I & 0\\ 0 & \sqrt{E' + E_V + 2}m_e v_F^2I \end{bmatrix} \Psi$$
(10)

This reduces to the form of a standard eigenvalue equation:

$$\left[\alpha_{x}\left(\partial_{x}+i\frac{|e|}{\hbar}A\right)-i\frac{|e|}{\hbar}\frac{\phi}{v_{F}}+\frac{1}{v_{F}}\partial_{\tau}\right]\Psi'=\frac{i}{\lambda}\Psi'$$
(11)

where $\lambda \equiv 1/(\hbar v_F)\sqrt{(E' + E_V)(E' + E_V + 2m_e v_F^2)} m^{-1}$. The Dirac matrix α_x is now the only one appearing in Equation (11). The progressive and regressive traveling wave solutions of Ψ' are eigenvectors pertaining to the eigenvalues \pm 1. In [1], in fact, it is shown that the spinor Ψ' is in the following form:

$$\Psi' = \begin{bmatrix} a+b\\ \sigma_x(a-b) \end{bmatrix}$$
(12)

where

$$a = \begin{bmatrix} a_0 \\ a_1 \end{bmatrix} \quad b = \begin{bmatrix} b_0 \\ b_1 \end{bmatrix} \tag{13}$$

Setting *b* = 0 in Equation (12) above retains just the progressive wave, as is required in this case. In the absence of y variation, moreover, we may set $a_0 = a_1 = a/\sqrt{2}$.

Since we are now dealing with just one eigenvector, in Equation (11), we may replace the matrix α_x with its eigenvalue +1 and reduce Equation (11) to an ordinary differential equation for the scalar a:

$$\left[\partial_{x} + i\frac{|e|}{\hbar\omega}\hat{A}\left(\omega - \frac{v^{2}}{v_{F}}k_{x}\right)e^{i(k_{x}x-\omega\tau)} + \frac{1}{v_{F}}\partial_{\tau}\right]a = \left[\frac{i}{\lambda} - \frac{1}{L_{F}}\right]a \tag{14}$$

It is expedient to introduce the "angular frequency"

$$\omega_1 \equiv v_F \frac{|e|}{\hbar} \hat{A} \frac{\omega - \frac{v^2 k_x}{v_F}}{\omega - v_F k_x}$$
(15)

and the position

$$\tilde{a} \equiv exp\left[-\omega_1/\omega e^{i(k_x x - \omega \tau)}\right]a\tag{16}$$

This reduces Equation (14) to the standard transmission line equation

$$\left[\partial_{x} + \frac{1}{v_{F}}\partial_{\tau}\right]\tilde{a} = \left[\frac{i}{\lambda} - \frac{1}{L_{F}}\right]\tilde{a}$$
(17)

The progressive wave solution of Equation (17) is

$$\tilde{a}(x,\tau) = exp\left[-\frac{x}{L_F} + \frac{i}{\lambda}(x - v_F\tau)\right]\tilde{a}(0,0)$$
(18)

with $\tilde{a}(0,0) = exp(-\omega_1/\omega)a(0,0)$. Finally, by introducing Equation (18) into Equation (16), we obtain the solution to Equation (14) as follows:

$$a(x,\tau;E') = exp\left[-\frac{x}{L_F} + \frac{i}{\lambda}(x - v_F\tau) + \frac{\omega_1}{\omega}\left(e^{i(k_xx - \omega\tau)} - 1\right)\right]a(0,0;E')$$
(19)

In addition, the original spinor Ψ is recovered by means of the inverse transformation of Equation (12):

$$\Psi = \begin{bmatrix} \frac{I}{\sqrt{E' + E_V}} & 0\\ 0 & \frac{I}{\sqrt{E' + E_V + 2m_e v_F^2}} \end{bmatrix} \Psi' = \frac{a}{\sqrt{2}} \begin{bmatrix} \frac{1}{\sqrt{E' + E_V}} \\ \frac{1}{\sqrt{E' + E_V}} \\ \frac{1}{\sqrt{E' + E_V + 2m_e + v_F^2}} \\ \frac{1}{\sqrt{E' + E_V + 2m_e + v_F^2}} \end{bmatrix}$$
(20)

Equation (19) shows that the R.F. produces frequency modulation as well as a timeretarded traveling wave in the phase of the spinor.

4. Definition of Current

From knowledge of the Dirac spinor Ψ , the general current density vector J(x, t; E') is defined as

$$J = -v_F |e| N(E') \Psi^{\dagger} \alpha \Psi \tag{21}$$

N(E') above is the electron density at the energy E', which is considered to be unaffected by the presence of the R.F. as is reasonable for moderate fields, as reported in [4]. Using Equation (18), the longitudinal component J_x is given by

$$Jx = -|e|Nv_F \Psi^{\dagger} \begin{bmatrix} 0 & \sigma_x \\ \sigma_x & 0 \end{bmatrix} \Psi = -2|e|Nv_F|a|^2 \left[\sqrt{(E'+E_V)(E'+E_V+2m_e v_F^2)} \right]^{-1}$$
(22)

However, Equation (19) gives

$$|a|^{2} = exp\left[-2\frac{x}{L_{F}} + 2\frac{\omega_{1}}{\omega}cos(k_{x}x - \omega t) - 1)\right]|a(0,0;E')|^{2}$$
(23)

Adopting the same current normalization as in [1], where $J(0,0;E') = -|e|N(E')v_F$, implies that $|a(0,0;E')|^2 = \frac{1}{2}\sqrt{(E'+E_V)(E'+E_V+2m_ev_F^2)}$ and consequently

$$J_x(x,t;E') = -|e|N(E')v_F \exp\left[-2\frac{x}{L_F} + 2\frac{\omega_1}{\omega}\cos(k_x x - \omega t) - 1)\right]$$
(24)

The first term in Equation (24) represents just d.c. losses in the absence of the R.F. signal. As a function of the frequency, the current shows high-pass characteristics. Moreover, there

appear to be infinite harmonics of the argument $\theta = k_x x - \omega t$, which is a feature of RF mixers. This fact is made explicit by the identity [2]

$$exp\left[2\frac{\omega_1}{\omega}\cos\theta\right] = \sum_k I_k\left(2\frac{\omega_1}{\omega}e^{ik\theta}\right) \qquad (k = 0, \pm 1, \pm 2, \ldots)$$
(25)

where $I_k(z) = i^{-k} J_k(iz)$ are the Bessel functions. Retaining only the fundamental harmonic of the signal (k = 1) yields the scalar admittance at the signal frequency.

We consider now a ballistic regime with flow in the x direction and which is uniform in the y direction. For a band of energies, the electron density N(E') is to be replaced by a density of states, weighted by the occupation probability and integrated from the thermodynamic energy limit $K_B T \approx 25$ meV at 300° up to the chemical potential μ . By retaining just the fundamental harmonic in Equation (24), this leads to a current density of

$$J = -2|e|v_F \frac{1}{L_x L_y} exp\left(\frac{2x}{L_F} + i\theta\right) I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega} \int_{K_B T}^{\mu} D(E')f(E')dE' \qquad [Am^{-1}]$$
(26)

The pre-factor 2, now appearing in Equation (26), is due to two electrons of opposite spins finding places in a state. Moreover, the density of the states is $D(E') = \frac{dN_S}{dk} \frac{dk}{dE'}$. Since we are considering a ribbon configuration, we assume the density of the states of a two-dimensional system with parabolic E-k characteristics first. The particular case of graphene will be considered presently.

Appearing in Equation (16) as well, $N_S = (\pi k^2) / (\frac{(2\pi)^2}{L_x L_y})$ is the number of states in the k-space and $E' = (\hbar k)^2 / (2m_e)$ such that:

$$D(E') = \frac{dN_S}{dk}\frac{dk}{dE'} = \frac{k}{2\pi}L_x L_y \frac{m_e}{\hbar^2 k} = L_x L_y \frac{m_e}{2\pi\hbar^2} = const.$$
 (27)

The probability of occupation, in the presence of the applied voltage V, is

$$f = \frac{1}{1 + exp[(E' - (\mu - \mu_0))/(K_B T)]}$$
(28)

where $\mu - \mu_0 = E_V$. Consistent with previous assumptions, we disregard the effect of the R.F. field energy on the probability distribution. The energy integral of Equation (26) is

$$J = -|e|\frac{v_F m_e}{\pi \hbar^2} exp\left(\frac{2x}{L_F} + i\theta\right) I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega} \Delta \qquad [Am^{-1}]$$
(29)

where, from the tables in [2] (p. 92), we have

$$\Delta = \int_{K_BT}^{\mu} f(E') dE' = \mu - K_B T \left[1 - ln \left(\frac{1 + e^{(K_B T - (\mu - \mu_0))/(K_B T))}}{1 + e^{E_V/(K_B T)}} \right) \right]$$
(30)

4.1. Graphene

Graphene provides an important particular case, since the dispersion relation is assumed to be of the type

$$E'(k) = (\hbar k)\frac{m_e v_F}{2m_e} = v_F \frac{\hbar k}{2}$$
(31)

This implies a density of states

$$D(E') = \frac{2E'}{\pi(\hbar v_F)^2} L_x L_y \qquad [J^{-1}].$$
(32)

In this case, Equation (29) is replaced by

$$J = -4\frac{|e|}{\pi\hbar^2 v_F} exp\left(\frac{2x}{L_F} + i\theta\right) I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega} \Delta' \qquad [Am^{-1}]$$
(33)

where

$$\Delta' \equiv \int_{K_B T}^{\mu} E' f(E') dE'$$
(34)

4.2. R.F. Quantum Admittance

The definition of admittance of the main harmonic is

$$Y(\omega) = -\frac{J}{E} \qquad [\Omega^{-1}] \tag{35}$$

In our case, $E = E_x = -\partial A/\partial t - \partial \phi/\partial x$, $\phi = v^2 k_x A/\omega$ is the scalar R.F. potential. The current propagation losses are now introduced in the potential. We have $\partial \phi/\partial x = (-2/L_F + ik_x)\phi$ and

$$E = i\omega A - \left(-\frac{2}{L_F} + ik_x\right)\phi = \frac{1}{i\omega}\left(v^2k_x^2 - \omega^2 + i\frac{2v^2k_x}{L_F}\right)A =$$

$$= \frac{1}{i\omega}\left(v^2k_x^2 - \omega^2 + i\omega\frac{2v}{L_F}\frac{n_e}{n}\right)A$$
(36)

In the last step, we used the fact that $vk_x = n_e/n\omega$, where n_e is the effective refractive index k_x/k_0 of the e.m. wave at the frequency in question and n = c/v. From Equations (26) and (29), at $x = L_x$, we find the following for the parabolic E-k dispersion:

$$Y(\omega) = -i\omega \frac{|e|v_F m_e \Delta}{\pi \hbar^2} e^{-2L_x/L_F} \frac{1}{\hat{A}} I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega} \left[v^2 k_x^2 - \omega^2 + i\omega \frac{2v}{L_F} \frac{n_e}{n}\right]^{-1}$$
(37)

whereas for the linear dispersion (graphene), we found the following (Equation (38)):

$$Y(\omega) = -i\omega \frac{|e|\Delta'}{\pi \hbar^2 v_F} e^{-2L_x/L_F} \frac{1}{\hat{A}} I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega} \left[v^2 k_x^2 - \omega^2 + i\omega \frac{2v}{L_F} \frac{n_e}{n}\right]^{-1}$$
(38)

Recalling that ω_1 is defined as in Equation(15), we find the following in the limit of the small argument:

$$Y(\omega) = -i\frac{|e|^{2}\Delta'}{\pi\hbar^{3}}e^{-2L_{x}/L_{F}}\frac{\omega - v^{2}k_{x}/v_{F}}{\omega - v_{F}k_{x}}\left[v^{2}k_{x}^{2} - \omega^{2} + i\omega\frac{2v}{L_{F}}\frac{n_{e}}{n}\right]^{-1}$$
(39)

If $n_e = n$, then $vk_x = \omega$, and thus:

$$Y(\omega) = -\frac{|e|^2 \Delta'}{\pi \hbar^3} e^{-2L_x/L_F} \frac{L_F}{2\omega v_F}$$
(40)

Figure 2 shows the admittance Y in the linear dispersion case in Equation (40) as functions of the frequency for different values of L_x , considering the parameters in Table 1. As is shown, as L_x approaches to the mean free path, the admittance decreases due to a transition between the ballistic and diffusive transport regimes.



Figure 2. Surface admittance in the low field limit considering the linear dispersion (graphene).

Parameter	Value
$v = v_F$	10 ⁶ m/s
μ_0	$4\pi imes 10^{-7}~{ m H/m}$
e	$1.602 imes 10^{-19} ext{ C}$
ħ	$1.055 imes10^{-34}~\mathrm{J~s}$
m_0	9.1110^{-31} kg
m_e	$0.06 \ m_0$
L_F	500 nm

The admittance of Equations (37) or (38) above is the admittance of a series RLC circuit seen through a frequency-dependent ideal transformer $n'(\omega)$:

$$Y(\omega) = \frac{j\omega C n^{\prime 2} \omega}{1 - \omega^2 L C + j\omega R C}$$
(41)

where j = -i, $LC = 1/(v^2k_x^2)$, $RC = (2v/L_F)(n_e/n)(1/(v^2k_x^2))$ and

$$Cn'^{2}(\omega) = \frac{|e|v_{F}m_{e}\Delta}{\pi\hbar^{2}v^{2}k_{x}^{2}}e^{-2L_{x}/L_{F}}\frac{1}{\hat{A}}I_{1}\left(\frac{2\omega_{1}}{\omega}\right)e^{-2\omega_{1}/\omega}$$
(42)

$$Cn^{\prime 2}(\omega) = \frac{|e|\Delta^{\prime}}{\pi\hbar^2 v^2 k_x^2 v_F} e^{-2L_x/L_F} \frac{1}{\hat{A}} I_1\left(\frac{2\omega_1}{\omega}\right) e^{-2\omega_1/\omega}$$
(43)

for the parabolic and linear dispersion cases, respectively.

In the small argument limit (weak field and high frequency), we have $I_1(z)e^{-z} \sim z/2$, whereas for large arguments (high field and low frequency), we have $I_1(z)e^{-z} \sim 1/\sqrt{2\pi z}$. In the former limit, recalling that ω_1 is defined as in Equation (15), we obtain

$$Cn'^{2}(\omega) = \frac{|e|^{2} v_{F}^{2} m_{e} \Delta}{\pi \hbar^{2} v^{2} k_{x}^{2}} e^{-2L_{x}/L_{F}} \frac{1}{\hbar \omega} \frac{\omega - (v^{2} k_{x})/v_{F}}{\omega - v_{F} k_{x}}$$
(44)

$$Cn^{\prime 2}(\omega) = \frac{|e|^2 v_F \Delta^{\prime}}{\pi \hbar^2 v^2 k_x^2 v_F} e^{-2L_x/L_F} \frac{1}{\hbar \omega} \frac{\omega - (v^2 k_x)/v_F}{\omega - v_F k_x}$$
(45)

for the parabolic and linear dispersion cases, respectively.

In the high field and low frequency limit, we obtain

$$Cn^{\prime 2}(\omega) = \frac{|e|v_F m_e \Delta}{\pi \hbar^2 v^2 k_x^2} \sqrt{\frac{\hbar \omega}{4\pi \hat{A}^3} |e|v_F} e^{-2L_x/L_F} \sqrt{\frac{\omega - v_F k_x}{\omega - (v^2 k_x)/v_F}}$$
(46)

$$Cn^{\prime 2}(\omega) = \frac{|e|\Delta^{\prime}}{\pi\hbar^2 v^2 k_x^2 v_F} \sqrt{\frac{\hbar\omega}{4\pi\hat{A}^3}} |e|v_F} e^{-2L_x/L_F} \sqrt{\frac{\omega - v_F k_x}{\omega - (v^2 k_x)/v_F}}$$
(47)

for the parabolic and linear dispersion cases, respectively.

Figure 3 shows the Cn^{2} dependence from the frequency in both the low-field and high-field as well as parabolic and linear approximations.



Figure 3. Comparison of the low-field (solid) and high-field (dashed) approximations for Cn^{2} in parabolic and linear dispersions.

A slightly more complex situation arises in presence of an R.F. TM wave with additional components E_z and H_v , but this is beyond the scope of the present work.

5. Conclusions

Starting from the four-component spinor from the Dirac equation, we derived a rigorous formulation of the quantum admittance for a monolayer 2D material at certain radio frequencies. A quantum-mechanical evaluation was then provided in the case of parabolic and linear dispersion in order to extract the frequency-dependent current density and thus the linear admittance. A subsequent analysis allowed us to extract an RLC-equivalent circuit with frequency-independent elements depending on the bias, temperature, effective mass, Fermi velocity and effective e.m. index of the material, losses and other relevant parameters. The circuit was evaluated while considering both low-field and high-frequency as well as high-field and low-frequency approximations.

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